INTRODUCTION

This application note presents an implementation of a data acquisition system based on a PIC14C000 microcontroller. The PIC14C000's analog front end will perform signal conditioning and analog to digital conversion of signals used in a battery monitoring application. Battery voltage, current, and temperature data will be acquired. This data will then be transmitted via RS-232 to a remote PC host.

SLOPE A/D CONVERSION

With the addition of an external capacitor, the analog front end of the PIC14C000 can be used as a slope A/D converter. The slope A/D is formed when a constant current source (CDAC pin) drives a capacitor. From basic capacitor theory, the voltage across this capacitor is described by the equation:

\[ V(t) = \frac{1}{C} \int_{t_0}^{t_1} i(t) \, dt \]

Since the current \( i(t) \) is constant, this reduces to:

\[ V(t) = \frac{1}{C} \times I(t_1 - t_0) \]

EQUATION 1: CAPACITOR VOLTAGE

This relationship describes a basic linear voltage ramp. The conversion from analog to digital occurs by measuring the time from the start of the linear ramp \( (t_0) \) to the time \( (t_1) \) that the voltage across the capacitor equals the analog input voltage to be converted. This time is measured by a digital counter circuit. Thus, the delta time \( (t_1 - t_0) \) value represents the magnitude of the analog voltage being converted. In this application note, the measured delta time value will simply be referred to as the "count" for the particular analog voltage being converted.

EQUATION 2: VOLTAGE RAMP

\[ V(t) - V_0 = \frac{1}{C} \times I(t_1 - t_0) \]

This magnitude of the measured analog voltage can be determined if the capacitance and the charging current are known. However, in practice, these values cannot be exactly determined. Therefore, a known reference voltage is used instead. This reference voltage is supplied by a very stable circuit known as a bandgap reference. The analog input voltage is determined ratiometrically by performing two successive A/D conversions, the first on the analog input voltage, and the second on the reference voltage. The analog voltage being measured can be calculated using the equation below.

\[ V_{IN} = \frac{N_{IN}}{N_{BG}} \times K_{BG} \]

EQUATION 3: VOLTAGE MEASURE

\( N_{IN} \) = A/D count value for selected input.
\( N_{BG} \) = A/D count value for bandgap reference.
\( K_{BG} \) = Absolute voltage value of the bandgap reference voltage, stored in calibration space EPROM.

Equation 3 assumes that the starting voltage of the linear ramp \( (V_0) \) in both the analog input and reference voltage conversions is zero. In practice, however, the capacitor cannot be discharged completely from the prior conversion and a few millivolts worth of charge,
referred to as offset voltage, may remain on the capacitor. This effect is called capacitor dielectric absorption, and varies depending on the capacitor’s dielectric material, the voltage to which it was charged during the last charge cycle, and the amount of time the capacitor has had to discharge. While teflon capacitors exhibit the lowest dielectric absorption, polystyrene and polyethylene are also very good. Ceramic, glass and mica are fair, and tantalum and electrolytic types are poor choices for A/D applications.

Additionally, the comparator (that compares the ramp voltage to the input voltage and stops the timer when the voltages are equal) usually has a few millivolts of offset error in its comparison. This comparator offset voltage adds (or subtracts) to the dielectric absorption offset. Finally, the counter that times the conversion may have a very small constant turn-on or turn-off delay that affects the measurement in the same manner as offset voltage.

In order to calculate an exact value for the analog input voltage, the various offset voltages must be factored into the equation. To do this, they are combined and measured.

The PIC14C000 provides two slope reference voltages for this purpose: upper and lower. The ratio of the magnitudes of these references is known and can be used to calculate the combined offset voltage.

This is done by performing conversions on both slope references, and using the supplied calibration constant for the ratio of their magnitudes, and calculating the offset voltage as an offset count. This offset count is then used in the other equations.

The equation used is that of calculating the x-intercept of a straight line when the slope of the line and two x coordinates are known.

**EQUATION 4: OFFSET COUNT**

\[
N_{\text{offset}} = N_{\text{reflo}} - K_{\text{ref}}(N_{\text{refhi}} - N_{\text{reflo}})
\]

Where:

- \(N_{\text{REFLO}}\) = A/D count value low reference point.
- \(N_{\text{REFHI}}\) = A/D count value high reference point
- \(K_{\text{REF}}\) = \(S_{\text{REFLO}} / (S_{\text{REFHI}} - S_{\text{REFLO}})\), stored in calibration space in EPROM.
- \(S_{\text{REFHI}}\) = See PIC14C000 Data Sheet, section 8.
- \(S_{\text{REFLO}}\) = See PIC14C000 Data Sheet, section 8.

This offset term and its measurement are illustrated graphically in Figure 2. Applying this offset term to the calculation of \(V_{IN}\) compensates the count obtained for both the input channel and the reference channel, to yield the counts as if each conversion did start from zero, instead of some offset voltage. Thus, the following equation may be used to determine the voltage at any input:

**EQUATION 5: VOLTAGE AT ANY INPUT**

\[
V_{IN} = \frac{N_{IN} - N_{\text{OFFSET}}}{N_{BG} - N_{\text{OFFSET}}} \times K_{BG}
\]

**RA1/AN1 and RD5/AN5 Analog Input Pins**

The AN1 and AN5 inputs pins have a special input offset feature that can allow these inputs to measure voltages that are either above or below device ground potential. This is accomplished with a summing junction that adds 0.5V to the signal at the pin before it reaches the A/D comparator. In order to determine the absolute voltage at the pin if the offset feature is turned on, two A/D conversions must be made. First, the input combined with the summing signal (0.5V) is converted. Then, a second conversion is performed with the AN1/AN5 side of the summing junction disconnected, resulting in just the 0.5V summing signal being converted. To compute the value of the voltage at the AN1/AN5 pin, the result from the second conversion is subtracted from the result of the first conversion.
FIGURE 2: FINDING THE ZERO VOLTAGE COUNT FROM \textit{S}\textsubscript{REFHI} AND \textit{S}\textsubscript{REFLO}

Projected count value for zero volt input.
IMPLEMENTATION

After initialization, the program continuously executes a 24 ms main loop. 16 ms is allocated for each A/D conversion, and 8 ms is allotted for calculations and other tasks. In order to conserve power and reduce noise in the A/D conversions, the CPU is put to sleep during each A/D conversion and during any unused portion of the 8 ms calculation time (Figure 3). This timing scheme allows both the charging time and the discharging time of the voltage ramp capacitor to be constant. This aids in achieving accurate A/D conversions by keeping the offset voltage due to capacitor dielectric absorption constant.

FIGURE 3: PROGRAM FLOW

Hardware Allocation

For this application note, three external analog input channels are used. RA1/AN1, RA2/AN2, and RA3/AN3 are assigned to battery current measurement, battery voltage measurement, and external voltage measurement (in this case a potentiometer), respectively.

Since the A/D converter measures voltage, and not current, the battery current measurement is obtained by measuring the voltage drop across a low value resistor (in this case 0.1 ohm). Actual battery current is then calculated by the firmware using the value of the resistor and Ohms law.

Battery voltage measurement requires that an external resistive voltage divider be used to lower the voltage input into the A/D converter’s range. A divider that results in an A/D input voltage that is as near as possible to the bandgap reference voltage is normally selected, since it reduces ratiometric errors during the calculation of the voltage. The firmware calculates the actual battery voltage from the voltage measured at the AN3 pin by multiplying the measured value by the external voltage divider ratio.

The external potentiometer voltage measurement is an auxiliary measurement, and could be used for measuring a thermistor, individual cell voltages, or other parameters. No scaling of this voltage is performed. The program simply reports the voltage sensed at the AN2 pin.

This program assumes that a 0.047 μF capacitor is connected between the CDAC pin of the device and ground. It is used for creating the ramp voltage for the A/D conversion process. Optionally, a 0.1 μF capacitor can be connected between the SUM pin and ground to allow for increased filtering of the battery current (AN1) input.

Port RC6 is used to transmit four parameters: battery current, battery voltage, internal temperature, and AN3 voltage. The format is 9600 baud (8,N,1) RS-232. Each parameter consists of four bytes and is in PICmicro™ 32-bit floating point format. Refer to AN575 for more information on floating point format.

For monitoring purposes, the program will toggle the RC5 output every ~384 ms. It will drive RC5 high just prior to starting the RS-232 data transmission, and drive it low after completing the transmission. If an LED and current limiting resistor are connected to RC5, a visible “heartbeat” indication will appear when the program is running in a normal manner.
A/D Conversion

The analog to digital conversion firmware modules control the operation of the analog to digital converter hardware. They convert the raw data received from the hardware into physical voltage values. This is accomplished by obtaining readings from the external inputs, the on-chip bandgap reference, and the on-chip A/D reference circuits. The physical voltages at the external inputs are computed based on these readings.

A/D Input Interleaving Sequence

Interleaving the selection of analog inputs scheduled for conversion maximizes the sampling rate for high priority signals such as the battery current, and reduces the sampling rate for low priority signals (that change at relatively slow rates), such as temperature inputs. The following interleaving scheme places the inputs in priority order from highest to lowest. Battery current is the highest priority with eight samples in 16 A/D cycles (~384 ms). Battery voltage is sampled two times in 16 A/D cycles. Battery temperature, via the external thermistor input and internal temperature, is sampled once each during 16 A/D cycles. Current network zero voltage, bandgap voltage, the A/D lower reference voltage, and the A/D upper reference voltage, are each sampled once for every 16 conversion cycles.

Conversions are scheduled at fixed intervals based upon the maximum conversion time to overflow (16 ms). This fixed scheduling method maintains determinism in the overall system.
TABLE 1: CONVERSION OPERATION TABLE

<table>
<thead>
<tr>
<th>Conv #</th>
<th>T_REL</th>
<th>T_ABS</th>
<th>Interleave Channel</th>
<th>A/D Channel</th>
</tr>
</thead>
<tbody>
<tr>
<td>0</td>
<td>16 ms</td>
<td>ms</td>
<td>Run sequence on current input channel</td>
<td>AN1: Ibat</td>
</tr>
<tr>
<td>1</td>
<td>16 ms</td>
<td>ms</td>
<td>Run sequence on V_REFHI channel</td>
<td>S_REFHI</td>
</tr>
<tr>
<td>2</td>
<td>16 ms</td>
<td>ms</td>
<td>Run sequence on current input channel</td>
<td>AN1: Ibat</td>
</tr>
<tr>
<td>3</td>
<td>16 ms</td>
<td>ms</td>
<td>Run sequence on V_REFLO channel</td>
<td>S_REFLO</td>
</tr>
<tr>
<td>4</td>
<td>16 ms</td>
<td>ms</td>
<td>Run sequence on current input channel</td>
<td>AN1: Ibat</td>
</tr>
<tr>
<td>5</td>
<td>16 ms</td>
<td>ms</td>
<td>Run sequence on Bandgap channel</td>
<td>V_BG</td>
</tr>
<tr>
<td>6</td>
<td>16 ms</td>
<td>ms</td>
<td>Run sequence on current input channel</td>
<td>AN1: Ibat</td>
</tr>
<tr>
<td>7</td>
<td>16 ms</td>
<td>ms</td>
<td>Run sequence on V_IN channel</td>
<td>AN3: Vbat</td>
</tr>
<tr>
<td>8</td>
<td>16 ms</td>
<td>ms</td>
<td>Run sequence on current input channel</td>
<td>AN1: Ibat</td>
</tr>
<tr>
<td>9</td>
<td>16 ms</td>
<td>ms</td>
<td>Run sequence on current zero channel</td>
<td>AN1: ZERO</td>
</tr>
<tr>
<td>10</td>
<td>16 ms</td>
<td>ms</td>
<td>Run sequence on current input channel</td>
<td>AN1: Ibat</td>
</tr>
<tr>
<td>11</td>
<td>16 ms</td>
<td>ms</td>
<td>Run sequence on internal thermistor channel</td>
<td>T_INT</td>
</tr>
<tr>
<td>12</td>
<td>16 ms</td>
<td>ms</td>
<td>Run sequence on current input channel</td>
<td>AN1: Ibat</td>
</tr>
<tr>
<td>13</td>
<td>16 ms</td>
<td>ms</td>
<td>Run sequence on external voltage channel</td>
<td>AN2: V_EXT</td>
</tr>
<tr>
<td>14</td>
<td>16 ms</td>
<td>ms</td>
<td>Run sequence on current input channel</td>
<td>AN1: Ibat</td>
</tr>
<tr>
<td>15</td>
<td>16 ms</td>
<td>ms</td>
<td>Run sequence on V_IN channel</td>
<td>AN3: Vbat</td>
</tr>
</tbody>
</table>

FIGURE 5: SEQUENCE FOR PERFORMING A SINGLE A/D CONVERSION

A/D Filtering
Due to the high resolution of the PIC14C000 A/D converter, digital filtering of the A/D count data is performed. This will reduce noise in the A/D readings, and enhance performance.

A/D count data is converted to PICmicro floating point format prior to being used in any calculation. All results are retained in floating point format as well. DC inputs such as bandgap reference voltage, slope reference high, slope reference low, and current zero offset voltage are filtered with long time-constant filters. Dynamic signals, such as battery voltage and current, are filtered less. Internal temperature and AN3 external voltage are not filtered at all. All calculated outputs are in voltage units. Figure 6 diagrams the data flow through the filtering and calculation task.

The formulas on the following page are used to filter the raw count data obtained from the A/D converter prior to calculating the actual voltage values for the A/D inputs. This filtering stabilizes the reference values to enhance A/D accuracy. The bandgap and offset reference are DC signals, so no information is lost by the filtering process.
The count value for the bandgap voltage reference is filtered by calculating the rolling average of the last 16 count values obtained. This filtered value of bandgap count is then used to calculate the input voltages. The subscript $i$ denotes the interleave sequence number, not the conversion number within the interleave sequence.

EQUATION 6: FILTERED BANDGAP COUNT

$$N_{fbg} = \frac{N_{BG,i} + 15 \times N_{BG,i-1}}{16}$$

The count offset value is filtered by calculating the rolling average of the last 16 count values obtained. The filtered value of the offset count is then used in Equation 6 to calculate the input voltages.
**Calculation of Input Voltage Values**

The following formulas are used to calculate the digital value for each of the input voltages.

**EQUATION 11: VOLTAGE AT AN1**

\[ V_{IBAT} = \frac{N_{IBAT} - N_{IZERO}}{Nfbg - Noffset} \times K_BG \]

\( V_{IBAT} \) refers to the voltage at the battery current input, AN1. Note that there is no \( N_{OFFSET} \) term in the numerator. The \( N_{OFFSET} \) components of the \( N_{IBAT} \) and \( N_{IZERO} \) terms are canceled out by the subtraction. The equations for the remaining inputs all follow the general form given in Equation 5.

**EQUATION 12: VOLTAGE AT AN0**

\[ VV_{BAT} = \frac{NfV_{BAT} - N_{OFFSET}}{Nfbg - N_{OFFSET}} \times K_BG \]

\( VV_{BAT} \) refers to the voltage at the battery voltage input, AN0. Additional filtering is added to the computed \( VV_{BAT} \) signal using the equation:

**EQUATION 13: FILTERED VOLTAGE**

\[ VV_{fBAT} = \frac{VV_{BAT} + 7 \times VV_{BAT}_{i-1}}{8} \]

Temperature terms are calculated directly without any added filtering.

**EQUATION 14: INTERNAL TEMPERATURE**

\[ VT_{INT} = \frac{NT_{INT} - N_{OFFSET}}{Nfbg - N_{OFFSET}} \times K_BG \]

\( VT_{INT} \) refers to the voltage at the internal temperature sensor.

**EQUATION 15: EXTERNAL TEMPERATURE**

\[ VT_{EXT} = \frac{NT_{EXT} - N_{OFFSET}}{Nfbg - N_{OFFSET}} \times K_BG \]

\( VT_{EXT} \) refers to the voltage at the external temperature sensor input.

**EQUATION 7: FILTERED OFFSET COUNT**

\[ N_{offset} = \frac{N_{OFFSET}_i + 15 \times N_{OFFSET}_{i-1}}{16} \]

where:

\[ N_{OFFSET}_i = N_{REFLO}_i - K_{REF}(N_{REFHI}_i - N_{REFLO}_i) \]

The current-input zero offset value is filtered by calculating the rolling average of the last 16 count values obtained. This filtered value of the current-input zero offset is used in the equation to calculate the input voltages.

**EQUATION 8: FILTERED ZERO-CURRENT**

\[ N_{IZERO} = \frac{N_{IZERO}_i + 15 \times N_{ZERO}_{i-1} + 1}{16} \]

The following formulas are used to filter the raw count data obtained from the battery voltage and current input channels. These filtered values are then used for communication and control functions.

The battery current value is filtered by taking the average of the eight samples of the input channel from the interleave sequence.

**EQUATION 9: FILTERED CURRENT COUNT**

\[ N_{fBAT} = \left( \frac{1}{8} \right) \sum_{s=0}^{7} (N_{BAT}_s) \]

The count value for the battery voltage input is filtered by calculating the average of two samples of the input channel from the interleave sequence.

**EQUATION 10: FILTERED VOLTAGE COUNT**

\[ N_{fVBAT} = \left( \frac{1}{2} \right) \sum_{s=0}^{1} (NV_{BAT}_s) \]
Conversion to Physical Units

The physical unit values (i.e., temperature, battery voltage, battery current) for the input voltages are computed prior to being transmitted via RS-232. To reduce data storage requirements, these values are not maintained in memory, but are destroyed after they are transmitted. Scaling constants read from EPROM are used to convert the voltage values measured at the pin into the appropriate physical value. The voltage at the AN2 pin is not scaled prior to transmission; the actual voltage at the pin is transmitted.

**Current**

\[ I_{BAT} = \frac{V_{BAT}}{R_{SENSE}} \]

- \( I_{BAT} \) = Battery current.
- \( V_{BAT} \) = measured voltage at RA1/AN1 pin.
- \( R_{SENSE} \) = External current sense resistor value (stored in user EPROM).

**Voltage**

\[ V_{BAT} = \frac{V_{fBAT}(V_{BAT}R_{DIV})}{298.15} \]

- \( V_{BAT} \) = Battery voltage.
- \( V_{fBAT} \) = Filtered measured voltage at RA3/AN3 pin.
- \( R_{DIV} \) = External resistor divider ratio for RA2/AN2 pin (stored in user EPROM).

**Temperature**

\[ T_{EMPINT} = \frac{V_{INT} - V_{therm}}{K_{TC}} + 298.15 \]

- \( T_{EMPINT} \) = Temperature in degrees Kelvin.
- \( V_{INT} \) = measured temperature sensor voltage value.
- \( V_{therm} \) = Factory calibrated voltage value of the temperature sensor at 298 Kelvin (stored in calibration place in EPROM).
- \( K_{TC} \) = Factory calibrated temperature constant of temperature sensor in volts per degrees Kelvin (stored in calibration space in EPROM).

RS-232 COMMUNICATION

The physical battery current, voltage, temperature, and RA3/AN3 voltage values are transmitted on the RC6 pin in 8,N,1 RS-232 format.

The transmit routine is designed to make use of the PIC14C000's calibrated internal (IN) oscillator. The oscillator frequency, stored in the factory calibration EPROM, is used as an index into a bit-delay lookup table. The bit-delay value controls the number of instructions executed during the software delay routine and is used to generate the time between bits being transmitted. The time resolution of this lookup table method results in a worst-case bit time error of less than two percent.

Several lookup tables for baud rate are included as assembly time options. Normally the 9600 baud option is used.

ASSEMBLY FILES

The program code for this application note is available on the Microchip BBS as the AN624.ZIP file. Once the file is unzipped, the user should read the README file for further instructions.
Note the following details of the code protection feature on PICmicro® MCUs.

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